

## §9. Poloidal Broadening of the Divertor Heat Flux Depending on the Radius of the Magnetic Axis

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The strike-point wetted area is quite important for determination of the heat flux flowing into the divertor plate. In an axisymmetric device such as a tokamak type, the wetted area can be simply calculated from a product of a width and a total length of the strike point along the torus. In a helical system, due to the difference of the rotation transform around divertor plates, the length of the strike point is usually longer than that of a comparable-size divertor tokamak. However, the width of the strike point is not uniform at different toroidal angles in helical devices; the divertor flux is located on particularly narrow areas.

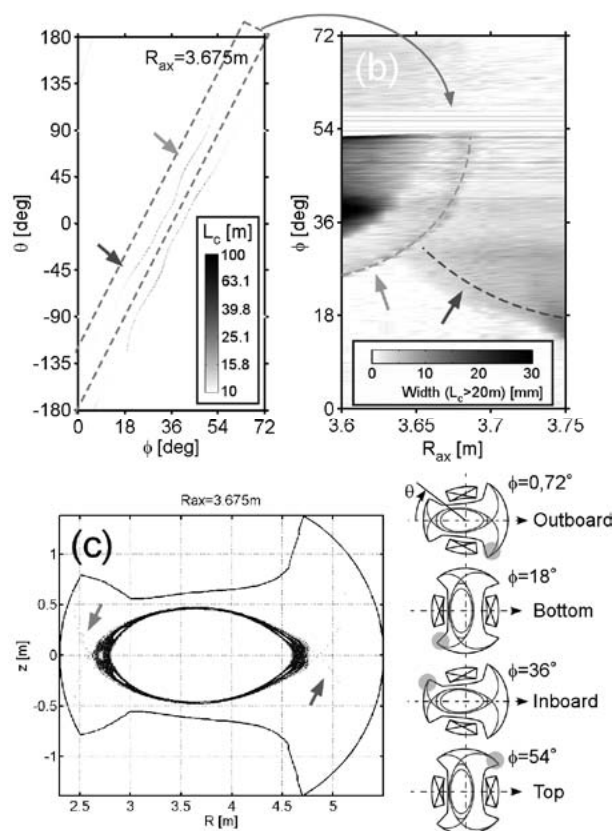


Fig. 1. (a)  $L_c$  distribution around the divertor plate for  $R_{ax} = 3.675$  m, (b) width of the  $L_c > 20$  m area, and (c) Poincaré plot of magnetic field lines for the horizontal-elongated cross-section for  $R_{ax} = 3.675$  m.

In the Large Helical Device (LHD), the divertor flux concentrates on the inboard-side divertor region in an inward shifted configuration of the magnetic axis position,  $R_{ax} \sim 3.6$  m<sup>1)</sup>. On the other hand, the deposition pattern moves to the upper and lower sides at  $R_{ax} \sim 3.75$  m. The past study<sup>2)</sup> indicated that there is a sudden change of the strike-point pattern at  $R_{ax} \sim 3.66$ – $3.67$  m. In this study, we have investigated the detailed relationship between the  $R_{ax}$  and the strike-point pattern from the magnetic field tracing; then,

we confirmed the calculation result with the Steady-State Operation (SSO) experiments.

Firstly, we have calculated magnetic-field connection length ( $L_c$ ) around the toroidally and poloidally rotating divertor plates at the minor radius of  $\sim 1.52$  m for several  $R_{ax}$  cases. Figure 1 (a) shows a  $L_c$  distribution with two strike points at  $R_{ax} = 3.675$  m as functions of the toroidal and the poloidal angles,  $\phi$  and  $\theta$ , respectively. From such figure, we estimated the width of long  $L_c$  area ( $L_c > 20$  m) as a function of  $\phi$  for  $R_{ax} = [3.6$  m,  $3.75$  m], as shown in Fig. 1(b). It can be found that there are two typical patterns having curves elongated from the inward and outward shifted  $R_{ax}$  positions. These patterns are strongly related to the X-point positions that release the divertor flux. At  $R_{ax} \sim 3.675$ – $3.68$  m, there is no thick strike point ( $> 10$  mm), but both the two patterns merges; length of the effective strike point along the torus becomes relatively long.

In the aim of decreasing a maximum temperature of divertor plates during a SSO discharge, broadening of the divertor flux in the poloidal direction is one of the valid procedures. To confirm the broadening effect, we measured temperatures inside the poloidally-distant divertor plates by thermocouples for  $R_{ax} = 3.65$  and  $3.675$  m, as shown in Fig. 2. By comparing these two cases, we concluded that there was a certain effect ( $\sim 10\%$ ) to reduce the maximum temperature.

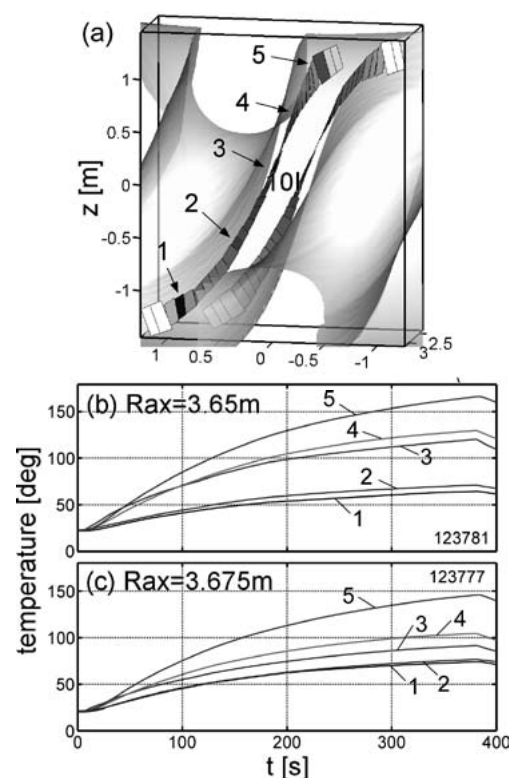


Fig. 2. (a) Divertor plates with a thermocouple. Time series of the divertor-plate temperatures during the same heating power shots for (b)  $R_{ax} = 3.65$  m and (c)  $3.675$  m.

- 1) Morisaki, T. et al.: Contrib. Plasma Phys. **42** (2002) 321.
- 2) Ogawa, H. et al.: Plasma Fusion Res. **2** (2007) 043.